

14-2. In general $\tilde{\mathbf{E}} = [E_{0x}e^{i\varphi_x}\hat{x} + E_{0y}e^{i\varphi_y}\hat{y}]e^{i(kz-\omega t)} = \begin{bmatrix} E_{0x}e^{i\varphi_x} \\ E_{0y}e^{i\varphi_y} \end{bmatrix} e^{i(kz-\omega t)} = \tilde{\mathbf{E}}_0$

(a) $\tilde{\mathbf{E}} = [E_0\hat{x} - E_0\hat{y}]e^{i(kz-\omega t)} \Rightarrow \tilde{\mathbf{E}}_0 = E_0 \begin{bmatrix} 1 \\ -1 \end{bmatrix} \Rightarrow \frac{1}{\sqrt{2}} \begin{bmatrix} 1 \\ -1 \end{bmatrix}$. Linearly polarized at -45° .

(b) $\tilde{\mathbf{E}} = [E_0\hat{x} + E_0\hat{y}]e^{i(kz-\omega t)} \Rightarrow \tilde{\mathbf{E}}_0 = E_0 \begin{bmatrix} 1 \\ 1 \end{bmatrix} \Rightarrow \frac{1}{\sqrt{2}} \begin{bmatrix} 1 \\ 1 \end{bmatrix}$. Linearly polarized at 45° .

(c) $\tilde{\mathbf{E}} = [E_0\hat{x} + E_0e^{-i\pi/4}\hat{y}]e^{i(kz-\omega t)} \Rightarrow \tilde{\mathbf{E}}_0 = E_0 \begin{bmatrix} 1 \\ e^{-i\pi/4} \end{bmatrix} \Rightarrow \frac{1}{\sqrt{2}} \begin{bmatrix} 1 \\ \frac{1}{\sqrt{2}}(1-i) \end{bmatrix}$. Then,

$$\tan 2\alpha = \frac{2E_{0x}E_{0y}\cos\epsilon}{E_{0x}^2 - E_{0y}^2} \rightarrow \infty \Rightarrow 2\alpha = 90^\circ, \alpha = 45^\circ$$

Right elliptically polarized at 45° .

(d) $\tilde{\mathbf{E}} = [E_0\hat{x} + E_0e^{i\pi/2}\hat{y}]e^{i(kz-\omega t)} \Rightarrow \tilde{\mathbf{E}}_0 = E_0 \begin{bmatrix} 1 \\ e^{i\pi/2} \end{bmatrix} \Rightarrow \frac{1}{\sqrt{2}} \begin{bmatrix} 1 \\ i \end{bmatrix}$. Left-circularly polarized.

14-3. In general $\tilde{\mathbf{E}} = [E_{0x}e^{i\varphi_x}\hat{x} + E_{0y}e^{i\varphi_y}\hat{y}]e^{i(kz-\omega t)} = \begin{bmatrix} E_{0x}e^{i\varphi_x} \\ E_{0y}e^{i\varphi_y} \end{bmatrix} e^{i(kz-\omega t)} = \tilde{\mathbf{E}}_0 e^{i(kz-\omega t)}$

(a) $\tilde{\mathbf{E}} = (2E_0\hat{x} + 0\hat{y})e^{i(kz-\omega t)} \Rightarrow \tilde{\mathbf{E}}_0 = 2E_0 \begin{bmatrix} 1 \\ 0 \end{bmatrix}$. Linearly polarized along the x -direction. Velocity is in the $+z$ -direction. The amplitude is $A = 2E_0\sqrt{1^2 + 0^2} = 2E_0$.

(b) $\tilde{\mathbf{E}} = (3E_0\hat{x} + 4E_0\hat{y})e^{i(kz-\omega t)} \Rightarrow \tilde{\mathbf{E}}_0 = E_0 \begin{bmatrix} 3 \\ 4 \end{bmatrix}$. The polarization direction makes the angle α with the x -axis where,

$$\alpha = \tan^{-1}(4/3) = 53^\circ$$

The wave is traveling in the $+z$ -direction with amplitude $A = \sqrt{3^2 + 4^2}E_0 = 5E_0$.

(c) $\tilde{\mathbf{E}} = 5E_0(\hat{x} - i\hat{y})e^{i(kz+\omega t)} \Rightarrow \tilde{\mathbf{E}}_0 = 5E_0 \begin{bmatrix} 1 \\ -i \end{bmatrix}$. The propagation is in the $+z$ -direction. The wave is right-circularly polarized with amplitude. The electric field vector traces out a circle of radius $5E_0$.

14-4. (a) $\tilde{\mathbf{E}}_1 = E_{01}(\hat{x} - \hat{y})e^{i(kz-\omega t)} \Rightarrow \tilde{\mathbf{E}}_{01} = 2E_{01} \begin{bmatrix} 1 \\ -1 \end{bmatrix}$. This is linearly polarized along -45°

$\tilde{\mathbf{E}}_2 = E_{02}(\sqrt{3}\hat{x} + \hat{y})e^{i(kz-\omega t)} \Rightarrow \tilde{\mathbf{E}}_{02} = E_{02} \begin{bmatrix} \sqrt{3} \\ 1 \end{bmatrix}$. This is linearly polarized along $\alpha = \tan^{-1}\left(\frac{1}{\sqrt{3}}\right) = 30^\circ$
The angle between the two is 75° .

(b) $\tilde{\mathbf{E}}_{01} \cdot \tilde{\mathbf{E}}_{02} = E_{01}E_{02}(\sqrt{3}-1) = (\sqrt{2}E_{01})(\sqrt{3+1^2}E_{02})\cos(\theta_{12}) \Rightarrow \cos\theta_{12} = \frac{\sqrt{3}-1}{2\sqrt{2}} \Rightarrow \theta_{12} = 75^\circ$

14-13. See Figure 14-13 that accompanies the statement of this problem in the text. Using the Jones formalism,

$$\begin{bmatrix} 1 & 0 \\ 0 & -i \end{bmatrix} \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ -i & -i \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 1 \\ -i \end{bmatrix} \quad \text{Right circular polarization}$$

QWP
SA, hor LP
at 45°

14-14. Using the Jones formalism,

$$\begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & i \end{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \quad \text{No light}$$

LP
TA vert HWP LP
TA hor QWP
FA hor LP
at 45°

14-17. Consider the action of the matrix on a general Jones vector,

$$\begin{bmatrix} 1 & i \\ -i & 1 \end{bmatrix} \begin{bmatrix} A \\ B+iC \end{bmatrix} = \begin{bmatrix} A+iB-C \\ -iA+B+iC \end{bmatrix} = (A-C+iB) \begin{bmatrix} 1 \\ -i \end{bmatrix}: \text{Right circular polarization}$$

For a left-circular polarizer try,

$$\begin{bmatrix} 1 & -i \\ i & 1 \end{bmatrix} \begin{bmatrix} A \\ B+iC \end{bmatrix} = \begin{bmatrix} A-iB+C \\ iA+B+iC \end{bmatrix} = (A+C-iB) \begin{bmatrix} 1 \\ +i \end{bmatrix}: \text{Left circular polarization}$$

14-18. Note that,

$$\underbrace{\begin{bmatrix} 1 \\ \pm i \end{bmatrix}}_{\text{Circular}} + \underbrace{\begin{bmatrix} \cos \alpha \\ \sin \alpha \end{bmatrix}}_{\text{Linear}} = \begin{bmatrix} \cos \alpha + 1 \\ \sin \alpha \pm i \end{bmatrix} = \underbrace{\begin{bmatrix} A \\ B \pm iC \end{bmatrix}}_{\text{Elliptical}}$$

6-(a) $\begin{pmatrix} -i \\ +i \end{pmatrix} = (-i) \begin{pmatrix} 1 \\ -1 \end{pmatrix}$, linearly polarized with $\alpha = -45^\circ$

6-(b) $\begin{pmatrix} -1+i \\ 1+i \end{pmatrix} = (-1+i) \begin{pmatrix} 1 \\ \frac{1+i}{-1+i} \end{pmatrix} = (-1+i) \begin{pmatrix} 1 \\ -i \end{pmatrix}$,
Right circularly polarized light.

6-(c) $\begin{pmatrix} -1-i \\ 1+i \end{pmatrix} = (-1-i) \begin{pmatrix} 1 \\ -1 \end{pmatrix}$, linearly polarized with $\alpha = -45^\circ$

6-(d) $\begin{pmatrix} i \\ i \end{pmatrix} = i \begin{pmatrix} 1 \\ -i \end{pmatrix}$, elliptically polarized ~~*~~

(1) Simply a linear polarizer with TAP (y)

$$M_{\text{linear}}(\text{TAP}(\hat{y})) = \begin{pmatrix} 0 & 0 \\ 0 & 1 \end{pmatrix}$$

or

$$M_{\text{linear}}(\theta = 90^\circ) = \begin{pmatrix} \cos^2 \theta & \cos \theta \sin \theta \\ \cos \theta \sin \theta & \sin^2 \theta \end{pmatrix}$$

then with $\vec{E}_{\text{inc}} = \begin{pmatrix} \alpha \\ \beta e^{i\Delta\phi} \end{pmatrix}$,

$$\begin{aligned} \vec{E}_{\text{out}} &= M_{\text{linear}}(\text{TAP}(\hat{y})) \vec{E}_{\text{inc}} \\ &= \beta e^{i\Delta\phi} \begin{pmatrix} 0 \\ 1 \end{pmatrix} \end{aligned}$$

The total energy is reduced from

$$(\alpha^2 + \beta^2) = 1$$

$$\text{to } \beta^2 \leq \alpha^2 + \beta^2 = 1 \quad \#$$

(2) Starting with a linear polarizer with
TA at 45° from x-axis,

$$M_{\text{linear}}(\theta=45^\circ) = \begin{pmatrix} \frac{1}{2} & \frac{1}{2} \\ \frac{1}{2} & \frac{1}{2} \end{pmatrix}$$

then the output from the linear polarizer

$$\vec{E}_{\text{out}}^{(1)} = M_{\text{linear}}(\theta=45^\circ) \vec{E}_{\text{in}}$$

$$= \frac{1}{\sqrt{2}} (\alpha + \beta e^{i\Delta\phi_0}) \begin{pmatrix} \frac{1}{\sqrt{2}} \\ \frac{1}{\sqrt{2}} \end{pmatrix}$$

Now for a left-circular polarized light,
we need to add $+\pi/2$ phase to the
y-component. We use a $\pi/4$ -plate
so oriented that

$$M_{\pi/4} = \begin{pmatrix} 1 & 0 \\ 0 & e^{i\pi/4} \end{pmatrix} = \begin{pmatrix} 1 & 0 \\ 0 & i \end{pmatrix}$$

$$\vec{E}_{\text{out}}^{(2)} = M_{\pi/4} \vec{E}_{\text{out}}^{(1)} = \frac{1}{\sqrt{2}} (\alpha + \beta e^{i\Delta\phi_0}) \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ i \end{pmatrix}$$

$$\left| \frac{1}{\sqrt{2}} (\alpha + \beta e^{i\Delta\phi_0}) \right|^2 \leq 1$$

If you start from the answer of part (a)

$$\vec{E}_{out} \sim (1) = \beta e^{i\delta\phi_0} \begin{pmatrix} 0 \\ 1 \end{pmatrix}$$

If we have a $\lambda/4$ plate set at $\theta = 45^\circ$, then

$$M_{\lambda/4}(\theta = 45^\circ) = \frac{1}{2} \begin{pmatrix} 1+i & -i \\ -i & 1+i \end{pmatrix}$$

then

$$\begin{aligned} \vec{E}_{out} \sim (2) &= \beta e^{i\delta\phi_0} \begin{pmatrix} 1-i \\ 1+i \end{pmatrix} \frac{1}{2} \\ &= \beta e^{i\delta\phi_0} e^{-i\pi/4} \begin{pmatrix} 1 \\ i \end{pmatrix} \frac{1}{\sqrt{2}} \end{aligned}$$

is a left-circularly polarized

If we start from $\begin{pmatrix} \alpha \\ 0 \end{pmatrix} = \alpha e^{i\delta\phi_0}$ and $M_{\lambda/4} = \begin{pmatrix} 1 & 0 \\ 0 & i \end{pmatrix}$
then $\vec{E}_{out} \sim (1)$ we use $\lambda/4$ at -45° :

$$M_{\lambda/4}(-45^\circ) = \frac{1}{2} \begin{pmatrix} 1+i & i-1 \\ i-1 & 1+i \end{pmatrix} \Rightarrow \vec{E}_{out} \sim \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ i \end{pmatrix}$$

(3) First use a wave-plate with arbitrarily adjustable phase

$$M_{\text{wp}}(\Delta) = \begin{pmatrix} 1 & 0 \\ 0 & e^{i\Delta} \end{pmatrix}$$

and choose $\Delta = -\Delta\phi_0$, then

$$\vec{E}_{\text{out}}^{(1)} = M_{\text{wp}}(\Delta = -\Delta\phi_0) \vec{E}_{\text{inc}}^{(1)}$$

$$= \begin{pmatrix} \alpha \\ \beta \end{pmatrix}, \quad \tan\theta = \beta/\alpha$$

They use a half-wave plate to rotate the linear polarized $\vec{E}_{\text{out}}^{(1)}$ into

$$\vec{E}_{\text{out}}^{(2)} = \begin{pmatrix} 0 \\ 1 \end{pmatrix} \left(M_{\lambda/2} = \begin{pmatrix} -\sin\Delta & \cos\Delta \\ \cos\Delta & +\sin\Delta \end{pmatrix} \right)$$

followed by a $\lambda/4$ -plate at $+45^\circ$

$$M_{\lambda/4}(+45^\circ) = \frac{1}{\sqrt{2}} \begin{pmatrix} 1+i & 1-i \\ 1-i & 1+i \end{pmatrix}$$

$$\Rightarrow \vec{E}_{\text{out}}^{(3)} = \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ i \end{pmatrix}, \quad \text{no loss of power.}$$

15-2. The polarizing angle is given by the relation, $\tan \theta_p = \frac{n_2}{n_1}$. So for $n_{\text{air}} = 1$ and $n_{\text{diam}} = 2.42$

$$\text{Internal reflection: } \theta_p = \tan^{-1} \left(\frac{n_{\text{air}}}{n_{\text{diam}}} \right) = \tan^{-1} \left(\frac{1}{2.42} \right) = 22.5^\circ$$

$$\text{External reflection: } \theta_p = \tan^{-1} \left(\frac{n_{\text{diam}}}{n_{\text{air}}} \right) = \tan^{-1} \left(\frac{2.42}{1} \right) = 67.5^\circ$$

15-4. $\frac{\lambda}{2} = t (\Delta n)$ or $t = \frac{\lambda}{2 \Delta n} = \frac{632.8 \times 10^{-7} \text{ cm}}{2(1.599 - 1.594)} = 0.063 \text{ mm}$

15-8. The angular offset between successive polarizers is $\theta = 90^\circ/N$. Applying Malus' law N times in succession,

$$I_T = I_0 (\cos^2 \theta)^N = I_0 [\cos(90^\circ/N)]^{2N} = 0.9 I_0$$

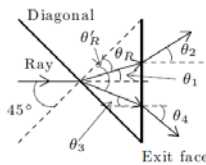
$$[\cos(90^\circ/N)]^{2N} = 0.9$$

A numerical solution indicates that N is between 23 and 24. For $N = 24$, $I_T = 0.9022 I_0$.

15-9. Using, $\lambda/4 = (\Delta n) t$,

$$t = \frac{\lambda}{4 \Delta n} = \frac{589.3 \times 10^{-6} \text{ mm}}{4(1.5534 - 1.5443)} = 0.0162 \text{ mm}$$

15-10. See Figure 15-24 that accompanies the statement of this problem in the text. Also refer to the figure below for the labeling of the various angles:



At the diagonal interface:

$$E_p \text{ component from } n_{\parallel} \text{ to } n_{\perp}: 1.4864 \sin 45 = 1.6584 \sin \theta_R \text{ or } \theta_R = 39.329^\circ$$

$$E_s \text{ component from } n_{\perp} \text{ to } n_{\parallel}: 1.6584 \sin 45 = 1.4864 \sin \theta'_R \text{ or } \theta'_R = 52.086^\circ$$

On exit:

$$\text{Upper ray: } \theta_1 = 45 - \theta_R = 5.671^\circ; 1.6584 \sin 5.671^\circ = (1) \sin \theta_2 \text{ or } \theta_2 = 9.432^\circ$$

$$\text{Lower ray: } \theta_3 = \theta'_R - 45 = 7.086^\circ; 1.4864 \sin 7.086^\circ = (1) \sin \theta_4 \text{ or } \theta_4 = 10.566^\circ$$

$$\text{Deviation: } \theta_2 + \theta_4 = 9.432^\circ + 10.566^\circ = 19.997^\circ \approx 20^\circ$$

15-12. See Figure 15-25 that accompanies the statement of the problem in the text.

(a) The incident angle is the polarizing angle,

$$\tan \theta_p = \frac{n_2}{n_1} = \frac{1.33}{1} \Rightarrow \theta_p = 53.12^\circ$$

(b) The angle θ_R the refracted ray makes with the normal to the air/water interface is

$$\theta_R = \sin^{-1} \left(\frac{\sin \theta_p}{1.333} \right) = 36.877^\circ$$

The polarizing angle for the water/glass interface is, $\theta'_p = \tan^{-1} \left(\frac{1.50}{1.333} \right) = 48.37^\circ$

If the glass surface was parallel to the water surface the angle of incidence on the glass would be $\theta_R = 36.877^\circ$. However, for complete polarization off the glass, θ'_p must be 48.37° . Thus the glass must be tilted by $48.37^\circ - 36.88^\circ = 11.5^\circ$ relative to the water surface.